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June 16, 2016 NTH Project No. 86-160105-200

Mayor Dennis Morley City of Eastlake Mayor's Office 35150 Lakeshore Boulevard Eastlake, Ohio 44060

RE: Geotechnical Engineering Services Galalina Storm Sewer Pump Station And Storm Sewer Improvements Eastlake, Ohio

Dear Mr. Morley:

We are pleased to submit this geotechnical exploration report performed for the proposed Galalina storm sewer pump station and storm sewer improvements. The purpose of this report is to present the results of our exploration for the project, including subsurface soil and groundwater conditions as well as construction considerations and recommendations for project design aspects. We provided our engineering services in general accordance with the agreed-upon scope of work outlined in our Proposal No. 86-160105, dated March 1, 2016.

We appreciate this opportunity to have been of service to you and trust the information provided in this report satisfies your present needs. If you have any questions, or if we may be of further assistance, please contact us.

Very truly yours,

NTH Consultants, Ltd.

Anthoni M. Fazio Senior Staff Engineer

cc: Brien Croff- CT Consultants, Inc.

Heather Audet, P.E. Senior Project Engineer



Mayor Dennis Morley June 16, 2016

1.0 PROJECT BACKGROUND

We understand that the City of Eastlake is planning to improve the Galalina storm sewer collection system. The planned improvements include a new pump station located at the intersection of Galalina Boulevard and Wacocka Drive as well as new storm sewers on Galalina Boulevard, Wacocka Drive, River Drive, Forest Drive, Matoma Boulevard, Wanaka Drive, Hillside and Hiawatha Boulevard. The depths of the storm sewers are expected to range from 6 to 10 feet, and the pump station is proposed to extend to a depth of approximately 15 feet below the existing ground surface.

2.0 GEOTECHNICAL EXPLORATION

For design of the new sewers and pump station, a geotechnical investigation program was performed over the period from May 2 through May 5, 2016. NTH and our drilling subcontractor, Ohio TestBor, Inc., mobilized to the project site, where we performed 11 test borings and installed three monitoring wells.

Prior to performing the test borings, clearances for underground utilities were obtained from the Ohio Utility Protection Service (OUPS) and the Oil and Gas Producers Underground Protection Service (OGPUPS) by NTH Consultants, Ltd. Test boring locations were staked in the field by NTH personnel. The test boring locations are shown on the Test Boring Location Plan, Figure No. 1 in the Appendix.

2.1 FIELD EXPLORATION

The test borings were drilled using a track-mounted drilling rig under the direct supervision of an NTH field engineer. Borings TB-1 through TB-11 were drilled at the location of the proposed pump station as well as along the alignments of the new sewers.



The test borings were advanced using 2¹/₄ -inch inside diameter hollow stem augers. Soil samples were obtained at 2.5-foot intervals to a depth of 10 feet and then at 5.0-foot intervals thereafter until termination depths of 15 feet were reached for TB-1 through TB-10 and 25 feet for TB-11.

Overburden soil samples were obtained using a standard split spoon sampler and the Standard Penetration Test (SPT) method. The SPT method (ASTM D-1586) consists of driving a 2½-inch inside diameter split-barrel sampler into the soil with a 140-pound weight falling freely through a distance of 30 inches. The sampler is generally driven three successive 6-inch increments, with the number of blows for each increment being recorded. The number of blows required to advance the sampler the last 12 inches is termed the Standard Penetration Resistance (N) and is presented on the individual logs of the test borings. As added information, the blow counts for each 6-inch increment are presented on the test boring logs. The automatic hammer on the rig was calibrated and reported to have an efficiency rating of 96 percent

Soil samples recovered from the split-barrel sampler are designated as "S" on the test boring logs. The soil samples obtained with the split-barrel sampler were sealed in jars and transported to our laboratory for further classification and testing. Samples obtained using the SPT method are generally considered disturbed.

In the field, an NTH engineer supervised the drilling procedures and performed the following specific duties: classified each sample recovered and preserved all recovered soil samples in airtight glass jar; prepared a log of each boring; made seepage and groundwater observations; and provided liaison between Ohio TestBor, Inc. and our Project Engineer so the exploration program could be modified in the event of unanticipated conditions.

General Notes defining the nomenclature used on the logs and elsewhere in this report are presented on Figure No.2. Individual Logs of Test Borings are presented on Figure Nos. 3 to 13. In addition to subsoil stratification, the test boring logs present Standard Penetration Test results, drilling and sampling information, and other pertinent data. The test boring logs included with this report have been prepared based on field and laboratory classification and testing.

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Within TB-6, 9 and 11, temporary groundwater monitoring wells were installed at the completion of drilling to evaluate static groundwater levels and conduct in-situ testing of the hydraulic properties of the granular soils located below the groundwater table. The wells were screened between the depths of 10 to 15 feet along the sewer alignment and 20 to 25 feet at the pump station. Logs of Monitoring Wells are presented in Figure Nos. 24 to 26. Slug testing was performed to determine the hydraulic conductivity of the native soils below the groundwater table to aid in evaluating ground water control measures during construction. The results can be seen in Section 4.3.

2.2 LABORATORY TESTING

Representative soil samples were subjected to laboratory testing to determine pertinent engineering characteristics of the subsurface soils. Testing included the determination of natural moisture content, Atterberg Limits, grain-size distribution using mechanical as well as hydrometer testing methods, dry density, unconfined compressive strength and loss on ignition to evaluate the content of organic matter. The results of the soil laboratory tests are presented on the Tabulation of Soil Test Data (Figure No. 14) and in the Logs of Test Boring. The results of grain-size distribution and hydrometer analyses (Figure Nos. 15 through 20).

3.0 SUBSURFACE CONDITIONS

Although the subsurface conditions encountered at the test boring locations varied somewhat, the general subsurface conditions encountered consist of asphalt pavement and base material underlain by native cohesive soils that are in turn underlain by native granular materials that extend to the explored depths.

The surficial materials at most of the explored locations consist of a 2 to 12-inch thick layer of asphalt underlain by 7 to 24 inches of gravel and sand base material. At the proposed pump station location, TB-11 was located outside of the pavement area and at this location the surficial materials consist of 5 inches of topsoil.

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Fill materials were encountered in TB-7 and TB-11 and extended to depths of approximately 3 feet at both locations. The fill materials encountered within TB-7 consisted of loose sand and gravel while the fill materials encountered at TB-11 consisted of medium compact clayey silt.

Beneath the surficial pavement and fill materials, the native soils are generally cohesive in nature and consist of soft to hard gray silty clay and clayey silt. At the boring locations, the cohesive soils extended to depths ranging from 3 feet to 8 feet below ground surface (bgs) with the exception of TB-10 where they extended to the explored depth of 15 feet.

The granular soils encountered below the cohesive soils consist of very loose to medium compact sand, sandy silt, clayey sand, silty sand, and sand and gravel. These soils generally extend to the termination of the borings. At the location of TB-11, a thin layer of silty clay was encountered directly below the granular materials, extending from a depth of 24¹/₂ feet to the termination depth of 25 feet.

Ground water was encountered at most of the test boring locations during drilling. In general, groundwater was encountered within the test borings at depths ranging between 4 to 10 feet which corresponds to elevations ranging from 571 to 566. Due to the granular nature of the subsurface materials the boreholes filled up with water quickly once the initial water table was reached. Borings TB-1, TB-2, TB-4, TB-5, TB-7, and TB-11 encountered artesian ground water conditions, with water rising to 2 to 3.5 feet bgs. Upon completion of drilling, the recorded groundwater levels correspond to elevations ranging from approximately 572.8 to 571.6. Specific water levels are available on the individual Log of Test Boring sheets attached to this report.

4.0 RECOMMENDATIONS AND CONCLUSIONS

We understand that open-cut construction methods are the preferred option for this project. Conclusions and recommendations pertaining to the design and construction of the proposed storm sewer pump station and storm sewer improvements are presented in the following paragraphs.



4.1 EARTHWORK CONSIDERATIONS

During earthwork operations, the contractor should be prepared to remove portions of the existing pavement that includes asphalt and gravel base. See individual Log of Test Boring sheets to determine asphalt thickness as it varies for each location. In areas where the proposed storm sewer improvements are located within the tree and lawn areas, the contractor should expect topsoil to be present at the ground surface.

Underneath the asphalt and gravel base the contractor should expect to encounter cohesive deposits of silty clay that range in consistency from medium to hard. The clayey soils are expected to extend to depths ranging from approximately 3.0 to 8.0 feet. Where excavations extend through the clayey soils, the underlying materials are expected to consist of granular deposits of sand, gravel or silt. Excavations that penetrate the overlying cohesive soils and extend into the granular materials should expect to encounter groundwater. At many of the test boring locations, the groundwater was noted to be artesian due to the confining nature of the clayey soils near the ground surface. As such any excavations that extend below Elevations on the order of 572.8 to 571.6, including those in clayey ground, should expect to encounter groundwater that will require a positive means of control before extending excavations below these depths.

4.2 STABILITY OF EXCAVATIONS

Based on the subsurface conditions encountered at the boring locations, we anticipate the majority of excavations will be performed through cohesive and wet granular soils. Based on our field exploration and laboratory test results, open cut construction methods appear feasible provided that appropriate positive means of groundwater control are utilized for any excavations that extend below the expected groundwater elevation in granular soils.

Excavations must be properly sloped or protected in accordance with OSHA requirements. In trenches and other excavations where there is inadequate space to allow for proper side slopes due to the presence of adjacent structures or utilities, temporary earth support should be provided using steel sheet piling. Appropriate trench box type excavation support systems can also be considered for shallow excavations.



Bracing systems for utility trenches may include portable trench boxes or sliding trench shields, provided groundwater control is undertaken. Otherwise, a watertight system will be required. In all cases, OSHA requirements must be followed and adequate protection provided for workers. Construction traffic and excavated material stockpiles should be kept away from excavations a minimum distance equal to the full depth of the excavation, unless the resulting surcharge loads are accounted for in the design of the lateral bracing system.

Based on the soil and groundwater conditions encountered, bottom instability and potential quick or heaving conditions are anticipated if the ground water is not controlled during excavation.

Extreme care must be exercised when making excavations close to surface and subsurface structures and utilities to prevent undermining or damage to the supported facilities. If excavations extend into the zone of influence of footings for any other structures, it will be necessary to provide temporary support to the existing footings during the time when excavations are open. Such temporary support measures could include temporary support systems, or underpinning of the existing footings adjacent to open excavations. The zone of influence of a footing may be considered to extend from the edge of the footing bottom in a downward direction at a slope of 1 unit horizontal to 1 unit vertical (1H:1V) away from the footing. Similarly, it will be necessary to provide temporary support to existing pavements if foundation or other excavations are made adjacent to or closely approach existing roadway pavements that are to remain.

4.3 GROUNDWATER CONTROL IN CONSTRUCTION EXCAVATIONS

On June 1, 2016 permeability testing was done for all monitoring wells within the granular soils. Table 1 below outlines the permeability coefficient (K) estimated using data from the slug tests. Figures 21 through 23 also present the graphical representation of slug testing data.



Location	Screen Elevation (ft)	Permeability (ft./sec				
MW-6	551-546	Silty Sand	2.7x10 ⁻⁵			
MW-9	551-546	Sandy Gravel and Silty	7.6x10 ⁻²			
		Sand				
MW-11	535-525	Sand and Gravelly	4.3x10 ⁻²			
		Sand				

Table 1 Permeability Coefficients

Based on the high permeability rate of the granular soils encountered at the boring locations, we anticipate significant groundwater inflow from the silt and sand layers into open cut excavations that extend below the groundwater table. Based on the relatively high permeability of the granular soils at the site as well as the relatively high groundwater table, we recommend that excavations extending below the groundwater table utilize a positive means of groundwater control such as well points to maintain the stability of trench bottoms and sides and prevent the migration of soil materials into excavations for the proposed sewers and pump station. The pump station excavation must be dewatered to prevent bottom instability and the use of a water-tight earth retention system is recommended to maintain a stable excavation.

4.4 TRENCH BEDDING AND BACKFILL

We anticipate the proposed storm sewer will be constructed using open cut methods. Trench bedding below and above the storm sewer should conform to the City of Eastlake requirements or the Ohio Department of Transportation 2013 Construction and Material Specifications (CMS) Section 603, entitled Pipe Culverts, Sewers, and Drains. The ODOT specification details the thickness and type of bedding and other information pertinent to the proposed construction. Due to the generally very loose to loose nature of the granular soils at the anticipated sewer invert level, the pipe installation trench should be excavated a minimum of 12 inches below the invert level of the pipe, loose native soils removed, and pipe bedding placed along the full width of the trench bottom. The pipe bedding should be ODOT Type 1 or Type 2 structural backfill and meet the requirements set forth in the ODOT standards and specifications for gradation and



compaction. The bedding materials should be clean and free of organics and other deleterious material and be properly compacted prior to placement of the pipe within the trench bottom.

If not addressed by the project or City specifications, we recommend compaction procedures and equipment for the pipe bedding is chosen based on ODOT Item of the 2013 CMS.

Based on the ODOT specifications for Item 603, we expect that the cohesive soils excavated for pipe construction will not meet the requirements for Type 1 and Type 2 structural fill and therefore will not be suitable for reuse as the bedding or backfill. The sand and gravel and sandy gravel layers meet the requirements of Type 1 and 2 backfill, however, we expect that these materials will be available in limited quantities. Due to their presence below the groundwater table, these materials may also require drying and conditioning so that they are at the optimum moisture content before being used as backfill.

4.5 LATERAL EARTH PRESSURES

As indicated earlier in this report, based on the prevailing site conditions and the anticipated depth of excavation on the order of 20 feet at the pump station, the use of internally braced soldier pile and lagging system with groundwater control or driven steel sheet piles for the earth retention system appears to be feasible for ground support. Such a system is considered to be flexible and will allow for some lateral movement. The amount of movement will depend on the spacing and stiffness of the structural members used and on the presence and spacing of the bracing levels.

Temporary earth support systems that are braced or cantilevered, should be designed by a licensed professional engineer that is experienced in evaluating temporary loading conditions associated with the soil and groundwater conditions at the pump station location. The system selected by the contractor should also consider an appropriate surcharge loading associated with equipment and materials that will be located near the excavation. For the permanent pump station, we expect that the walls of the structure will be generally fixed against lateral movement due to external soil and hydrostatic loading. As such, we recommend that the walls for the structure be designed on the basis of "at rest" earth pressure conditions. Accordingly, an equivalent fluid pressure of 60 psf/ft



may be used for the portion of the walls above the design groundwater level. Below the groundwater level, an equivalent fluid pressure of 90 psf/ft should be used for design of the walls. As indicated earlier in this report, we recommend the groundwater level should be treated as being at the ground surface for purposes of permanent wall design. If long terms surcharge loads are expected due to adjacent activities, these should also be evaluated and included in the permanent lateral load for the structure.

4.6 PUMP STATION FOUNDATION CONSIDERATIONS

Based on an overall evaluation of the subsurface data developed during the course of this investigation as well as the available data regarding the proposed construction, the pump station invert will be located near the interface of the loose gray sand and the underlying medium compact gravelly sand. Due to the loose nature of the soils to a depth of 17 feet, we recommend that the pump station be founded on the medium compact gravelly materials located below Elevation 559. The proposed pump station may be supported on a structural slab or mat foundation bearing on the gravelly sand or upon properly compacted engineered fill that extends from the recommended bearing material. A net allowable bearing pressure of 3000 pounds per square foot (psf) may be used for the design of the foundation for the support of the proposed structure. The applied gross bearing pressure for a pump station should be calculated based on the weight of the structure including the slab or mat foundation, the contents of the structure, and backfill over the structure, plus any external live loads that may act on the structure.

The granular soils encountered at the proposed pump station invert level during our field exploration could lose stability when overworked by construction equipment and foot traffic or if ground water control is not continued during construction. Therefore, we recommend that once the required bearing materials has been achieved and any required engineered fill placed, that the bottom of the excavation be covered with a layer of coarse aggregate to minimize disturbance of the bearing soils and provide a stable base during the floor construction. Alternatively, a thin mud mat can be constructed to serve as a working platform and also to help stabilize the bottom of the excavation.



In addition to bearing capacity considerations, the foundation design process should also consider whether the total weight of the structure is adequate to withstand the uplift forces resulting from hydrostatic pressures from the accumulation of groundwater within the backfill. We recommend the factor of safety against buoyancy be a value of 1.1 or greater. If the weight of the empty structure is not adequate to resist the hydrostatic uplift forces with an adequate factor of safety, consideration may be given to increasing the plan dimensions of the floor slab / mat foundation so that the foundation projects beyond the walls of the structure. The purpose of such a projection would be to engage the soil (backfill) surrounding the structure so that the weight of the soil would contribute to resisting the uplift forces. Another approach to providing an adequate factor of safety against buoyancy is to increase the floor slab and/or top slab thickness to increase the dead weight of the structure sufficiently. This approach may be used in combination with enlarging the floor slab / mat foundation to project beyond the walls of the structure.

The determination of the required depth of excavation at the foundation location should be performed by a qualified representative of the geotechnical engineer. The foundation excavation should be carefully observed and tested to verify that adequate in-situ soil bearing pressures compatible with the design value are achieved.

If the recommendations outlined in this report are followed, total settlement of the structure is expected to be less than one inch, and differential settlement is expected to be on the order of one-half of the total settlement, provided that the foundation is adequately reinforced and constructed to be sufficiently rigid. In general, increasing the reinforcement and rigidity of the foundation will decrease the differential settlement.

Based on our review of the conditions encountered in the test borings, as well as our knowledge of regional geology in the area, the site may be classified as Site Class E in accordance with the 2013 Ohio Building Code.

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5.0 DATA REVIEW AND FIELD MONITORING

The evaluations and recommendations presented in this report relative to site preparation and structure support have been formulated on the basis of the information provided and/or the assumptions stated herein relating to the proposed project. Any significant changes in this information should be brought to our attention for review with respect to the prevailing subsurface conditions.

Our experience indicates that the actual subsoil conditions at a site may vary from those generalized on the basis of test borings made at specific locations. Therefore, we recommend that an experienced geotechnical engineer be retained to provide soil engineering services during the site preparation, excavation, and foundation installation. This is to observe compliance with the design concepts, specifications, and recommendations. Also, field monitoring allows design changes to be made in a timely manner in the event that subsurface conditions differ from those anticipated prior to the start of construction.

After the foundation designs have been completed, the geotechnical engineer should be retained and provided the opportunity to review the final design plans and specifications to check that our engineering recommendations have been properly incorporated into the design documents. At this time, it may be necessary to submit supplementary recommendations. If NTH is not retained to perform these functions, NTH will not be responsible for the impact of those conditions on the project. This report has been prepared for the exclusive use CT Consultants, Inc. and the City of Eastlake for the specific application to the proposed Galalina pump station and storm sewer improvements.

6.0 REPORT LIMITATIONS

This report is specifically intended for the design of the proposed Galalina pump station and storm sewer improvements in Eastlake, Ohio. The work was performed in accordance with the prevailing standard of practice in this area at the time the work was performed. No other warranty, express or implied, is provided or intended.

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Soil samples obtained during this exploration will be held at our Valley View, Ohio office for 90 days. At that time, CT Consultants, Inc. will have the option to take possession of the samples for continued storage, or we will make arrangement for sample disposal.

The scope of services for this exploration was limited to an evaluation of subsurface conditions for the determination of foundation design for the pump station and storm sewer improvements. The recommendations presented in this report are based on the findings at the 11 soil borings located within the proposed project location. It must be understood that variations between borings can occur. Should significantly different subsurface conditions be encountered during construction, NTH should be contacted immediately to assess the impact of these changes on our recommendations. No environmental surveys, hydrological studies or chemical testing or analyses were performed as part of this geotechnical exploration.





APPROXIMATE LOCATION OF TEST BORINGS DRILLED BY OHIO TESTBOR, INC. UNDER THE SUPERVISION OF NTH CONSULTANTS, LTD. MAY 2 THROUGH MAY 5, 2016

	NIH CONSULTANTS, LTG.		
CAD FILE NAME: 86-160105	INCEP DATE: MAY 2016	DRAWING SCALE: AS SHOWN	PLOT DATE: MAY 2016
NTH PROJECT No.: 86-160105	DESIGNED BY: AF	DRAWN BY: TG	снескер ву: HA
TEST BORING LOCATION PLAN	STORM SEWER IMPROVEMENTS	CALALINA PUMP STATION	EASTLAKE, OHIO
FIG	URE	No.	

NTH Consultants, Ltd.

A Neyer, Tiseo & Hindo Company

GENERAL NOTES

TERMINOLOGY

Unless otherwise noted, all terms utilized herein refer to the Standard Definitions presented in ASTM D 653.

PARTICLE SIZES

CLASSIFICATION

The major soil constituent is the principal noun, i.e., clay, silt, sand, gravel. The second major soil constituent and other minor constituents are reported as follows:

Boulders Cobbles Gravel - Coarse Fine	 Greater than 12 inches (305mm) 3 inches (76.2mm) to 12 inches (305mm) 3/4 inches (19.05 mm) to 3 inches (76.2mm) No. 4 - 3/16 inches (4.75mm) to 3/4 inches (19.05 mm) 	Second Major Constituent (percent by weight)	Minor Constituents (percent by weight)
Sand - Coarse	 No. 10 (2.00mm) to No. 4 (4.75mm) 	Trace - 1 to 12%	Trace - 1 to 12%
Medium Fine	 No. 40 (0.425mm) to No. 10 (2.00mm) No. 200 (0.074mm) to No. 40 (0.425mm) 0.025mm to 0.074mm 	Adjective - 12 to 35% (clayey, silty, etc.)	Little - 12 to 23%
Silt Clay	 0.005mm to 0.074mm Less than 0.005mm 	(Clayey, Silly, etc.)	Some - 23 to 33%
		And - Over 35%	

COHESIVE SOILS

If clay content is sufficient so that clay dominates soil properties, clay becomes the principal noun with the other major soil constituent as modified; i.e., silty clay. Other minor soil constituents may be included in accordance with the classification breakdown for cohesionless soils; i.e., silty clay, trace of sand, little gravel.

Consistency	Unconfined Compressive <u>Strength (psf)</u>	Approximate <u>Range of (N)</u>
Very Soft	Below 500	0 - 2
Soft	500 - 1000	3 - 4
Medium	1000 - 2000	5 - 8
Stiff	2000 - 4000	9 - 15
Very Stiff	4000 - 8000	16 - 30
Hard	8000 - 16000	31 - 50
Very Hard	Over 16000	Over 50

Consistency of cohesive soils is based upon an evaluation of the observed resistance to deformation under load and not upon the Standard Penetration Resistance (N).

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	COHESIONLESS SOILS	
Density	Relative	Approximate
<u>Classification</u>	Density %	<u>Range of (N)</u>
Very Loose	0 - 15	0 - 4
Loose	16 - 35	5 - 10
Medium Compact	36 - 65	11 - 30
Compact	66 - 85	31 - 50
Very Compact	86 - 100	Over 50

Relative density of cohesionless soils is based upon the evaluation of the Standard Penetration Resistance (N), modified as required for depth effects, sampling effects, etc.

SAMPLE DESIGNATIONS

- AS Auger Sample directly from auger flight BS Miscellaneous Sample bottle or bag S Split Spoon Sample ASTM D 1586

- LS Split Spoon Sample S with Liner Insert 3 inches in length ST Shelby Tube Sample 3 inch diameter unless otherwise noted
- PS Piston Sample 3 inch diameter unless otherwise noted
- RC Rock Core NX core unless otherwise noted
- CS Continuous Sample from rock core barrel or continuous sampling device
- VS Vane Shear

STANDARD PENETRATION TEST (ASTM D 1586) - A 2.0" outside-diameter, 1-3/8" inside-diameter, split barrel sampler is driven into undisturbed soil by means of a 140-pound weight falling freely through a vertical distance of 30 inches. The sampler is normally driven three successive 6-inch increments. The total number of blows required for the final 12 inches of penetration is the Standard Penetration Resistance (N).

Project Name: Galalina Pump Station Project Location: Eastlake, Ohio



NTH Consultants, Ltd. NTH Proj. No.: 86-160105-200 Checked By:

Γ				SUBSURFACE PROFILE					SOI	_ SAM	PLE D	ATA		
	ELEV. (FT) 575	PRO- FILE	ELEV	GROUND SURFACE ELEVATION: 575.0	DEPTH	DEPTH (FT)	SAMPLE TYPE/NO.	BLOWS/ 6-INCHES	STD. PEN RESIST. (N)	REC (in)	FIELD TEST (ppm)	MOIST. CONTENT (%)	DRY DENSITY (PCF)	UNCONF. COMP ST (PSF)
F		000	574.8	ASPHALT	0.2									
-	-	· 0 ·	,	GRAVEL Base			-							
		Pool	573.0		2.0			10 4						
		$ \mathcal{N} $	572.0	Very Stiff Gray SILTY CLAY	3.0		S-1	4	7	16				*5000
-	- - 570		572.0		0.0		S-2	1 2 3	5	9				5000
	-		1				-	2						
F	-			Loose to Very Loose Gray SILTY SAND			<u>S-3</u>	3	4	8				
ŀ	565					10	S-4	2	3	7				
ŀ	-		563.5		11.5									
	-			Medium Compact Gray SAND			-	5 8						
L	560		560.0	END OF BORING AT 15.0 FEET.	15.0	15	S-5	7	15	12				
CORPORATE.GDT 5/31/16	- 5555 - - - - - - - - - - - - - - - -													
LOG OF TEST BORING 86-160105-200.GPJ NTH CORPORATE.GDT 5/31/16	Drillin Drillin Inspector Drille Drillin 2 1, Plugg Bac	ractor: ng Meti /4" HSA ging Pr ckfilled	t Date: Date: A Mobile ocedure with bei	15 FT 5/4/16 5/4/16 A. Fazio Ohio TestBor, Inc. D. Hepner B-57 track-mounted rig e: ntonite grout, and pavement repaired using	Grc 2'2' Note: * =	undwa " upon o s: pocket	complet penetro	ountere tion. ometer	value	during c	trilling,	and end	counter	ed at
LOG C	cole	d patch			Аррі	oximat	te GPS	Cooral	nates:			Fig	jure No	o. 3



NTH Consultants, Ltd. NTH Proj. No.: 86-160105-200

Project Name: Galalina Pump Station Project Location: Eastlake, Ohio

Projec	t Locat	ion:	Eas	tlake, Ohio			1		C	Checke	d By:	WS		
				SUBSURFACE PROFILE					SOII	SAN	IPLE D	ATA		
ELEV. (FT)	PRO- FILE	E	LEV	GROUND SURFACE ELEVATION: 575.0	DEPTH	DEPTH (FT)	SAMPLE TYPE/NO.	BLOWS/ 6-INCHES	STD. PEN RESIST. (N)	REC (in)	FIELD TEST (ppm)	MOIST. CONTENT (%)	DRY DENSITY (PCF)	UNCONF. COMP ST (PSF)
575		57	4.5	ASPHALT	0.5									
		10	2.5	GRAVEL Base	2.5		S-1	10 7 4	11	6				
570		57	70.0	Stiff Dark Gray CLAYEY SILT, Trace Sand, Intermittent Sand Layers	5.0	5	S-2	3 4 5	9	16				*3000
		54	67.0	Soft Gray SILTY CLAY, Trace Organics	8.0		S-3	1 1 2	3	15				*3000
565			57.0		0.0	10	S-4	1 2 1	3	8			-	*3000
				Very Loose to Loose Gray SILTY SAND Blowing Sand at 12'			-							
560		56	50.0	END OF BORING AT 15.0 FEET.	15.0	15	S-5	2 3 5	8	10				*3000
				15 FT				vation:						
Drill Drill Insp Con Drill Drill	ing Sta ing En ector: tractor er: ing Me	art [d D :: tho	ate:	5/6/16 5/6/16 A. Fazio Ohio TestBor, Inc. D. Hepner 9-57 track-mounted rig	3′5 Note	" upon s:	comple			during	drilling,	and en	counter	ed at
Plug Ba	ging P	Proc d wi	edure		Арр	roxima	te GPS	Coordi	nates:			Fig	gure N	o. 4

Project Name: Galalina Pump Station Project Location: Eastlake, Ohio



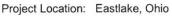
NTH Consultants, Ltd.

NTH Proj. No.: 86-160105-200

Checked By:

			SUBSURFACE PROFILE					SOIL	SAM	PLE D	ATA		
ELEV (FT)		ELEV	GROUND SURFACE ELEVATION: 576.0	DEPTH	DEPTH (FT)	SAMPLE TYPE/NO.	BLOWS/ 6-INCHES	STD. PEN RESIST. (N)	REC (in)	FIELD TEST (ppm)	MOIST. CONTENT (%)	DRY DENSITY (PCF)	UNCONF. COMP ST (PSF)
	601	575.7	ASPHALT	0.3	-								
575	-000	10	GRAVEL Base			-							
-	-200	573.7		2.3		-	7						
570			Stiff Gray SILTY CLAY		 	S-1 S-2	3 1 1 2 1	6	18				*3000
-						S-3	1 2	3	18				*4500
- - 565		568.0	Very Loose Gray SANDY SILT, Trace Clay	8.0	10	S-4	1 1 1	2	18				
-	-		Very Loose Gray SAND, Trace Clay				3 2						
560		561.0	END OF BORING AT 15.0 FEET.	15.0	15	S-5	2	4	12				
OKING 86-160105-200.GPJ N Dri Dri Dri Dri Dri Dri 2	al Depti lling Sta lling En pector: ntractor ller: lling Me 1/4" HS	art Date d Date: :: :thod:	15 FT : 5/6/16 5/6/16 A. Fazio Ohio TestBor, Inc. D. Hepner ile B-57 track-mounted rig	Gro rea Note	oundwa ding up s:	Observator enco	ountere npletion		during	drilling.	No grou	undwate	ər
Plu B C	gging F ackfilled old patc	d with b	re: entonite grout, and pavement repaired using	Арр	roxima	te GPS	Coordi	nates:			Fig	gure No	o. 5

Project Name: Galalina Pump Station





NTH Consultants, Ltd.

NTH Proj. No.: 86-160105-200

Checked By:

			SUBSURFACE PROFILE					SOI	L SAM	PLE D	ATA		
ELEV. (FT) 575	PRO- FILE	ELEV	GROUND SURFACE ELEVATION: 575.0	DEPTH	DEPTH (FT)	SAMPLE TYPE/NO.	BLOWS/ 6-INCHES	STD. PEN RESIST. (N)	REC (in)	FIELD TEST (ppm)	MOIST. CONTENT (%)	DRY DENSITY (PCF)	UNCONF, COMP ST (PSF)
		574.4	ASPHALT	0.6									
	000	573 5	GRAVEL Base	1.5		-							
	MA D	010.0	Stiff Brown SILTY CLAY, Little Sand,	1.0			3						
-	1/II				F -	1	3 2 2	122					ne and rener
L -		572.0	Trace Organics	3.0	L .	S-1	2	4	18				*2500
570			Very Loose Brown SANDY SILT, Little Clay		5	S-2	1 1 1	2	18				
	. / .	569.0		6.0	L .								
						<u>S-3</u>	1 2 1	3	18				
	1.						1						
505	1/				- 40		1	~	10				
565	1		Very Loose Coarse SILTY SAND And		10	S-4	2	3	10				
			GRAVEL			-							
	1.1	1			L.		1						
560	1.1.1	560.0		15.0	15	S-5	1	2	12				
5555 5555 5555 5555 5550 5550 5550 555			END OF BORING AT 15.0 FEET.										
7 Total	Depth		15 FT	Wate	rlave	Obser	vation			A			
0 Duill	Depth	+ Datas		vvale	Level	tor one	valion:	date	durina	drillin	and -	a a um t	ad at
g Drilli	ng Star	t Date:	5/3/16	Gro	undwa	uer enc	ountere	a at 6' i	auring a	ırılıng,	and end	counter	ea at
Drilli	ng End	Date:	5/3/16	2'6'	" upon	comple	tion.						
E Inspe	ector:		C. Fellows										
Cont	ractor:		Ohio TestBor, Inc.	2000 00									
brille			D. Hepner	Notes	s:								
		h a al c	D. Hepher			nenotr	ometer	value					
	ng Met	nod:		_	POUNDI	penetr	0110101	-uluc					
8 21	/4" HSA	A Mobile	B-57 track-mounted rig										
ă													
	ging Pr	ocedure	e:										
H Ra			ntonite grout, and pavement repaired using										
Lo go o	d patch		nonne grout, and pavement repaired Using	Арри	roxima	te GPS	Coordi	nates:			Fig	gure No	o. 6

Project Name: Galalina Pump Station Project Location: Eastlake, Ohio



NTH Consultants, Ltd.

NTH Proj. No.: 86-160105-200

Checked By:

b SOIL SAMPLE DATA SUBSURFACE PROFILE MOIST. CONTENT (%) DRY DENSITY (PCF) STD. PEN RESIST. FIELD UNCONF. COMP ST GROUND SAMPLE TYPE/NO. BLOWS/ 6-INCHES ELEV. (FT) DEPTH REC PRO-DEPTH ELEV FILE (FT) (in) SURFACE ELEVATION: 575.0 (N) (ppm) (PSF) 575 ASPHALT 574.6 0.4 1.0 574.0 GRAVEL Base And Slag Medium Gray SANDY CLAY, Some Silt 22 *2000 572.0 3.0 S-1 4 18 1 570 5 S-2 2 13 Very Loose Gray SILTY SAND, Trace 2 18 27.4 S-3 Clay, Trace Gravel 2 22 10 S-4 4 10 565 564.0 11.0 Very Loose SILTY SAND, Little Gravel, Trace Clay 2 1 18 19.1 15 S-5 3 560 560.0 15.0 END OF BORING AT 15.0 FEET. 555 550 NTH CORPORATE.GDT 6/9/16 545 540 Total Depth: 15 FT Water Level Observation: GPJ Groundwater encountered at 5' during drilling, and encountered at **Drilling Start Date:** 5/4/16 86-160105-200. **Drilling End Date:** 5/4/16 2'4" upon completion. A. Fazio Inspector: Contractor: Ohio TestBor, Inc. Notes: D. Hepner Driller: * = pocket penetrometer value BORING **Drilling Method:** 2 1/4" HSA Mobile B-57 track-mounted rig **Plugging Procedure:** Backfilled using cement grout, and pavement repaired using Approximate GPS Coordinates: OG OF cold patch Figure No. 7

FST

Project Name: Galalina Pump Station Project Location: Eastlake, Ohio



NTH Consultants, Ltd.

NTH Proj. No.: 86-160105-200

UNCONF. COMP ST

(PSF)

*5000

101.1 *1660

Checked By: IN to

SOIL SAMPLE DATA SUBSURFACE PROFILE MOIST. CONTENT (%) DRY DENSITY (PCF) STD. PEN RESIST. FIELD GROUND DEPTH SAMPLE TYPE/NO. BLOWS/ 6-INCHES ELEV. (FT) REC PRO-ELEV DEPTH FILE (FT) (in) SURFACE ELEVATION: 576.0 (N) (ppm) ASPHALT 575.6 0.4 575 Very Stiff Gray SILTY CLAY 4 23 17 3.0 S-1 5 573.0 1 22 16 Medium Gray SILTY CLAY 5 S-2 4 26.4 570 569.5 6.5 1 2 3 17 S-3 1 10 S-4 2 16 23.9 Very Loose Gray SILTY SAND, Trace Clay 565 and Gravel 15.0 15 S-5 3 5 561.0 END OF BORING AT 15.0 FEET. 560 555 550 545 Water Level Observation: **Total Depth:** 15 FT Drilling Start Date: Groundwater encountered at 6'. No groundwater reading upon 5/5/16 Drilling End Date: 5/5/16 completion. Inspector: A. Fazio Ohio TestBor, Inc. Contractor: Notes: Driller: D. Hepner * = pocket penetrometer value **Drilling Method:** 2 1/4" HSA Mobile B-57 track-mounted rig **Plugging Procedure:** Monitoring well installed. Approximate GPS Coordinates:

OG OF TEST BORING 86-160105-200.GPJ NTH CORPORATE.GDT 5/31/16



NTH Consultants, Ltd.

			SUBSURFACE PROFILE				1	SOIL	SAM		DATA		
ELEV. (FT)	PRO- FILE	ELEV	GROUND SURFACE ELEVATION: 575.0	DEPTH	DEPTH (FT)	SAMPLE TYPE/NO.	BLOWS/ 6-INCHES	STD. PEN RESIST. (N)	REC (in)	FIELD TEST (ppm)	MOIST. CONTENT (%)	DRY DENSITY (PCF)	UNCON COMP : (PSF)
575		574.6	ASPHALT	0.4									
-	00 • ^ • ^	100 million (100 million (100 million))	GRAVEL Base	1.5			7						
-		572.0	Fill: Loose Brown Coarse SAND And GRAVEL, Some Clay	3.0		S-1	5 4	9	18				
570		569.5	Very Soft Brown SANDY SILT, Some Clay	5.5	5	S-2	1 1 1	2	18				*50
-		568.5	Very Loose Coarse Brown SAND and	6.5	1	-	1/18"						
-	1	567.5	GRAVEL Very Soft Gray SANDY SILT	7.5		S-3	-		18				< *50
- 565					10	S-4	1 2 2	4	16				
_			Loose Gray Coarse SILTY SAND And GRAVEL			-							
_							2 3						
560	1	560.0	END OF BORING AT 15.0 FEET.	15.0	15	S-5	2	5	18				
550 545													
- - - 540	-												
Total Drilli Drilli Inspe Cont Drille Drille	ng End ector: ractor: er: ng Met	rt Date d Date: hod:	5/3/16 C. Fellows Ohio TestBor, Inc. D. Hepner	Gra 2'1 Note	oundwa 0" upoi • s:	ater enc n comp		ed at 5' d value	during	drilling,	and en	counter	red a
Plug	ging P ckfillea	rocedu	ile B-57 track-mounted rig I re: uttings and pavement repaired with cold	Арр	roxima	te GPS	Coordi	inates:			- ;	gure N	~ (

Project Name: Galalina Pump Station



NTH Consultants, Ltd. NTH Proj. No.: 86-160105-200 Checked By:

Project Location: Eastlake, Ohio

			SUBSURFACE PROFILE					CHES RESIST. (N) REC (in) TEST (ppm) CONTENT (ppm) 5 4 2 6 1 2 1 2 0H 1 2 18	1		1		
ELEV. (FT)	PRO- FILE	ELEV	GROUND SURFACE ELEVATION: 575.0	DEPTH	DEPTH (FT)	SAMPLE TYPE/NO.	BLOWS/ 6-INCHES	RESIST.		TEST	MOIST. CONTENT (%)	DRY DENSITY (PCF)	UNCONF. COMP ST (PSF)
575		574.6 574.0 572.5	ASPHALT SAND Base Very Stiff Gray SANDY CLAY	0.4 1.0 2.5		S-1	5 4 2	6	18				*5500
570		569.0	Very Soft Gray SILTY CLAY	6.0		S-2	1 1 1	2	18				*500
		567.0	Very Soft Gray SANDY SILT, Some Clay	8.0		<u>S-3</u>	WOH 1 1	2	18				< *500
565					 10	S-4	1 2 3	5	14				
			Very Loose to Loose Gray SILTY SAND and GRAVEL			-							
560		560.0	END OF BORING AT 15.0 FEET.	15.0	15	S-5	2 3 1	4	18				
	-												
<u>555</u> 	-												
550	-												
	-												
	-												
Tota Drilli Drilli Inspo Cont	ector:	rt Date d Date:	5/3/16 C. Fellows Ohio TestBor, Inc.	Gro end	oundwa counter	Obser ater enc ed upor	ountere	ed at 6.5 letion.	5' durin	g drillin	g. No gr	oundw	ater
Drille Drilli	er: Ing Met	thod:	D. Hepner ile B-57 track-mounted rig	Note * =		penetr	ometer	value					
Ba		rocedu I with ci	re: uttings and pavement repaired with cold	Арр	roxima	te GPS	Coordi	nates:			Figu	ire No	. 10

Project Name: Galalina Pump Station



NTH Consultants, Ltd. NTH Proj. No.: 86-160105-200 Checked By:

Project Location: Eastlake, Ohio

RO- ILE ELEV 575.0 573.0	GROUND SURFACE ELEVATION: 576.0 ASPHALT Medium Gray SILTY CLAY	DEPTH	DEPTH (FT)	SAMPLE TYPE/NO.	BLOWS/ 6-INCHES	STD. PEN RESIST. (N)	REC (in)	FIELD TEST (ppm)	MOIST. CONTENT (%)	DRY DENSITY (PCF)	UNCON COMP S (PSF)
										3	
573.0	Medium Gray SILTY CLAY										
		3.0		S-1	8 5 2	7	17				*150
I L		0.0		_	WOH WOH						
	Very Soft Gray CLAYEY SILT, Trace Sand, Trace Organics		5	S-2	1 W O	0	17		66		< *50
568.5		7.5		S-3	H	0	18				< *50
	Loose Dark Gray SANDY GRAVEL, Trace Clay			S-4	2 2 2	4	15		14.5		
564.0		12.0		-							
561.0	Loose Dark Gray SILTY SAND	15.0	 	S-5	WOH	4	11				
/ 001.0	END OF BORING AT 15.0 FEET.	10.0	10								
epth: Start Date	15 FT :: 5/5/16	Gro	oundwa	ter enc	ountere	d at 10'	during	drilling	. No gro	oundwa	ter
End Date: or: tor: Method:	5/5/16 A. Fazio Ohio TestBor, Inc. D. Hepner	Note	s:								
		App	roximat	te GPS	Coordi	nates:					
SED IT	pth: Start Date End Date: r: or: Method: J Procedu	Clay 564.0 Loose Dark Gray SILTY SAND 561.0 END OF BORING AT 15.0 FEET. pth: 15 FT Start Date: 5/5/16 End Date: 5/5/16 r: A. Fazio or: Ohio TestBor, Inc. D. Hepner	Clay 564.0 12.0 Loose Dark Gray SILTY SAND 561.0 15.0 END OF BORING AT 15.0 FEET. Phi: 15 FT Wate 564.0 12.0 Value of the second	S64.0 12.0 Loose Dark Gray SILTY SAND 15.0 S61.0 15.0 END OF BORING AT 15.0 FEET. 15.0 Phi: 15 FT Water Level Groundwa Sant Date: 5/5/16 Soft Date: 5/5/16 Or: Ohio TestBor, Inc. D. Hepner *= pocket *SA Mobile B-57 track-mounted rig Procedure: intoring Well to 15'.	Clay 10 04 Loose Dark Gray SILTY SAND 12.0 S61.0 15.0 15 END OF BORING AT 15.0 FEET. 15.0 15 S61.0 15.0 15 S51.0 END OF BORING AT 15.0 FEET. 15.0 S61.0 15.0 15 S51.0 END OF BORING AT 15.0 FEET. 15.0 S61.0 Image: Signal Content of Signal Conten	Loose Dark Gray SANDY GRAVEL, Trace Clay 10 S-4 2 564.0 12.0 12.0 12.0 Loose Dark Gray SILTY SAND 15.0 15 S-5 3 END OF BORING AT 15.0 FEET. 15.0 15 S-5 3 Ph: 15 FT Water Level Observation: Groundwater encountere encountered upon compler; or: Ohio TestBor, Inc. D. Hepner Water Level Observation: Groundwater encountere encountered upon complex * = pocket penetrometer * = pocket penetrometer * = pocket penetrometer * = pocket penetrometer	Loose Dark Gray SANDY GRAVEL, Trace Clay Loose Dark Gray SILTY SAND Loose Dark Gray SILTY SAND Set.0 Loose Dark Gray SILTY SAND Set.0 Loose Dark Gray SILTY SAND Set.0	Loose Dark Gray SANDY GRAVEL, Trace 10 5-4 2 4 15 564.0 12.0 12.0 10 5-4 2 4 15 10 5-4 2 4 15 15 5-5 3 4 11 10 END OF BORING AT 15.0 FEET. 15.0 15 5-5 3 4 11 10 END OF BORING AT 15.0 FEET. 15.0 15 5-5 3 4 11 11 END OF BORING AT 15.0 FEET. 15.0 15 5-5 3 4 11 11 END OF BORING AT 15.0 FEET. 15.0 15 5-5 3 4 11 11 END OF BORING AT 15.0 FEET. 15.0 15 15 16 16 17 16 17 16 16 17 16 17 17 16 17 17 17 17 17 16 17 17 17 17 16 17 17 17 11 17 17 17 17 17 17 17 17 <td>Loose Dark Gray SANDY GRAVEL, Trace 10 5.4 2 4 15 564.0 12.0 10 5.4 2 4 15 Loose Dark Gray SILTY SAND 12.0 15 5.5 3 4 11 561.0 15.0 15 5.5 3 4 11 END OF BORING AT 15.0 FEET. 15.0 15 5.5 3 4 11 pth: 15.7 15 15 15 16 16 start Date: 5/5/16 5/5/16 5 5 10' during drilling encountered upon completion. 10' during drilling encountered upon completion. 10' during drilling encountered upon completion. * = pocket penetrometer value * = pocket penetrometer value * 15 Procedure: * = pocke</td> <td>Loose Dark Gray SANDY GRAVEL, Trace Clay 10 8-4 2 4 15 14.5 564.0 12.0 12.0 10 8-4 2 4 15 14.5 Loose Dark Gray SILTY SAND 15.0 15 8-5 3 4 11 END OF BORING AT 15.0 FEET. 15.0 15 8-5 3 4 11 Phi: 15.7 7 7 14.5 14.5 Phi: 15.7 7 8 14.5 11 Phi: 15.7 7 7 10 11 11 Phi: 15.7 7 7 7 10 10 10 10<td>Loose Dark Gray SANDY GRAVEL, Trace Clay 64.0 Loose Dark Gray SILTY SAND Loose Dark Gray SILTY SAND Loose Dark Gray SILTY SAND 5510 END OF BORING AT 15.0 FEET. WOH 15.0 15. 55 4 11 WOH 11 WOH 11 WOH 11 WOH 11 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 16. 17. 17. 17. 18. 19. 10.</td></td>	Loose Dark Gray SANDY GRAVEL, Trace 10 5.4 2 4 15 564.0 12.0 10 5.4 2 4 15 Loose Dark Gray SILTY SAND 12.0 15 5.5 3 4 11 561.0 15.0 15 5.5 3 4 11 END OF BORING AT 15.0 FEET. 15.0 15 5.5 3 4 11 pth: 15.7 15 15 15 16 16 start Date: 5/5/16 5/5/16 5 5 10' during drilling encountered upon completion. 10' during drilling encountered upon completion. 10' during drilling encountered upon completion. * = pocket penetrometer value * = pocket penetrometer value * 15 Procedure: * = pocke	Loose Dark Gray SANDY GRAVEL, Trace Clay 10 8-4 2 4 15 14.5 564.0 12.0 12.0 10 8-4 2 4 15 14.5 Loose Dark Gray SILTY SAND 15.0 15 8-5 3 4 11 END OF BORING AT 15.0 FEET. 15.0 15 8-5 3 4 11 Phi: 15.7 7 7 14.5 14.5 Phi: 15.7 7 8 14.5 11 Phi: 15.7 7 7 10 11 11 Phi: 15.7 7 7 7 10 10 10 10 <td>Loose Dark Gray SANDY GRAVEL, Trace Clay 64.0 Loose Dark Gray SILTY SAND Loose Dark Gray SILTY SAND Loose Dark Gray SILTY SAND 5510 END OF BORING AT 15.0 FEET. WOH 15.0 15. 55 4 11 WOH 11 WOH 11 WOH 11 WOH 11 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 16. 17. 17. 17. 18. 19. 10.</td>	Loose Dark Gray SANDY GRAVEL, Trace Clay 64.0 Loose Dark Gray SILTY SAND Loose Dark Gray SILTY SAND Loose Dark Gray SILTY SAND 5510 END OF BORING AT 15.0 FEET. WOH 15.0 15. 55 4 11 WOH 11 WOH 11 WOH 11 WOH 11 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 15. 16. 17. 17. 17. 18. 19. 10.

Project Name: Galalina Pump Station Project Location: Eastlake, Ohio



NTH Consultants, Ltd.

NTH Proj. No.: 86-160105-200

Checked By:

SOIL SAMPLE DATA SUBSURFACE PROFILE DRY DENSITY (PCF) UNCONF. COMP ST (PSF) STD. PEN RESIST. FIELD MOIST. CONTENT GROUND DEPTH SAMPLE TYPE/NO. BLOWS/ 6-INCHES REC ELEV. (FT) PRO-ELEV DEPTH FILE (FT) (in) SURFACE ELEVATION: 575.0 (N) (ppm) (%) 575 ASPHALT 574.0 1.0 1.5 SAND Base 573 544 18 16.6 >*9000 S-1 8 4 67 S-2 18 >*9000 570 5 13 4 5 6 S-3 18 116.9 >*8280 11 15.3 Hard Brown SILTY CLAY, Little Sand And **Fine Gravel** 4 67 18 >*9000 565 10 S-4 13 357 15 S-5 12 18 >*9000 15.0 560 560.0 END OF BORING AT 15.0 FEET. 555 550 LOG OF TEST BORING 86-160105-200.GPJ NTH CORPORATE.GDT 6/16/16 545 540 **Total Depth:** 15 FT Water Level Observation: Drilling Start Date: Drilling End Date: 5/3/16 No groundwater encountered upon completion. 5/3/16 Inspector: C. Fellows Contractor: Ohio TestBor, Inc. Notes: Driller: D. Hepner * = pocket penetrometer value **Drilling Method:** 2" OD SS, Standard **Plugging Procedure:** Monitoring well installed. Approximate GPS Coordinates:

Figure No. 12

Project Name: Galalina Pump Station

Project Location: Eastlake, Ohio



NTH Consultants, Ltd.

NTH Proj. No.: 86-160105-200

Checked By:

		1	SUBSURFACE PROFILE					SOIL	SAM	PLE D	ATA		1
ELEV. (FT)	PRO- FILE	ELEV	GROUND SURFACE ELEVATION: 576.0	DEPTH	DEPTH (FT)	SAMPLE TYPE/NO.	BLOWS/ 6-INCHES	STD. PEN RESIST. (N)	REC (in)	FIELD TEST (ppm)	MOIST. CONTENT (%)	DRY DENSITY (PCF)	UNCO COMP (PSF
575		575.5	Topsoil CLAYEY SILT	0.5							-		
- 10		573.0	FILL: Medium Compact Brown CLAYEY SILT, Trace Sand	3.0		S-1	5 6 6	12	15				
		570.5	Medium Gray SILTY CLAY, Trace Sand	5.5	5	S-2	1 1 1	2	17				*20
570						S-3	WOH 1 1	2	18		32.2	88.8	*80
_			Very Soft Gray SANDY SILT, Little Clay		- · ·		WOH 1 1	2	17		41.5		
565		564.0		12.0		-							
-			Loose Gray SAND, Trace GRAVEL		15	S-5	3 3 4	7	5				
560	~	559.0		17.0		_							
-	Medium Compact Gray GRAVELL		20	S-6	4 6 6	12	12		12.8				
<u>555</u> - -	0.00		SAND, Trace Clay and Silt			-	5						
	NV	551.5 551.0	Gray SILTY CLAY	24.5 25.0	25	S-7	6 6	12	15				
550			END OF BORING AT 25.0 FEET.	_									
545	-												
	-												
Drilli Drilli Inspe	ng End	rt Date: Date:	25 FT 5/4/16 5/4/16 A. Fazio	Gro	oundwa	l Obser ater enc pletion.	ountere	ed at 5' o	during	drilling a	and end	ountere	ed a
Drille Drilli	ng Met	hod:	Ohio TestBor, Inc. D. Hepner e B-57 track-mounted rig	Note: * =		t penetr	ometer	value					
		oring we		Арр	roxima	te GPS	Coordi	inates:				ure No	

PROJECT NO. 86-160105-200

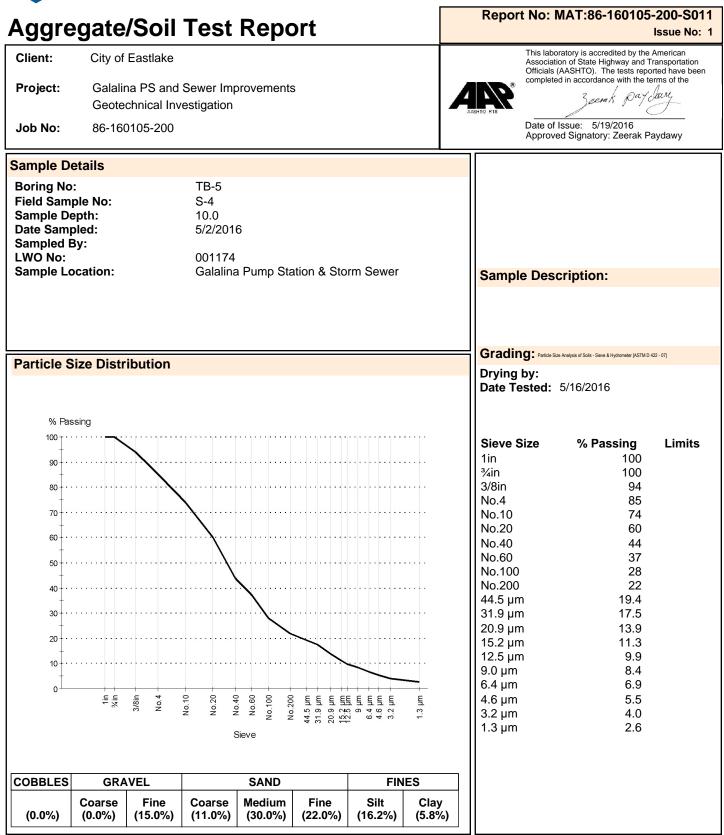
NTH CONSULTANTS, LTD.

SHEET 1 OF 1

	TABULATION OF LABORATORY SOIL TEST DATA																			
7		୍କ	LE	Strength	(lTΥ	sec)	PAI	RTICLE	SIZE D	ISTRIBU	TION (S	%)		TERBE MITS (9		FIC	(%	
BORING / TEST PIT / PROBE DESIGNATION	SAMPLE NUMBER	DEPTH OF SAMPLE TIP (FT)	ELEVATION OF SAMPLE TIP (FT)	UNCONFINED COMPRESSIVE STRE (PSF)	FAILURE STRAIN (%)	NATURAL WATER CONTENT (% OF DRY WEIGHT)	IN-PLACE DRY DENSITY (LBS/CU.FT)	Permeability (cm/sec)	CLAY	SILT	FINE SAND	MEDIUM SAND	COARSE SAND	GRAVEL	L ΙαυΙΡ LΙΜΙΤ	PLASTIC LIMIT	PLASTICITY INDEX	APPARENT SPECIFIC GRAVITY	LOSS ON IGNITION (%)	UNIFIED SOIL CLASSIFICATION
B-5 B-5	S-3 S-4	7.5 10	567.5 565	-	-	27.4 19.1	-		- 5.8	- 16.2	- 22	- 30	- 11	- 15	- -	-	-	-	-	-
B-6 B-6	S-2 S-4	5 10	571 566	1660 -	15 -	26.4 23.9	101.1 -		- 6.8	- 14.2	- 45	- 16	13	- 5	- -	- -	-	-	-	-
B-9 B-9	S-3 S-4	7.5 10	568.5 566	-	-	66.0 14.5	-		23.4 ←	73.6 8	2 7	1 19	0 19	- 47	-	-	-	-	6.2 -	-
B-10 B-10	S-1 S-3	3 10	572 565	- 8280	- 8.9	16.6 15.3	- 116.9		-	-	-	-	-	-	-	-	-	-	-	-
B-11 B-11 B-11	S-3 S-4 S-6	7.5 10 20	568.5 566 556	800 - -	15 - -	32.2 41.5 12.8	88.8 - -		- 15.9 (55.1	- 26 9	- 3 23	- 0 22	- 0 35	27 -	20 -	7	-	-	-

FIGURE NO. 14







•	~ ~ (~ 1)		Report No: MAT	:86-160105-200-S011
Aggre	gate/s	Soil Test Report		Issue No: 1
Client:	City of Ea	astlake	Association of S Officials (AASH	s accredited by the American tate Highway and Transportation IO). The tests reported have been
Project:		PS and Sewer Improvements nical Investigation		cordance with the terms of the 3 cera k Pay chury
Job No: 86-160105-200			Date of Issue: Approved Sig	5/19/2016 natory: Zeerak Paydawy
Sample De	tails			
Boring No: Field Samp Sample De Date Samp Sampled B LWO No: Sample Loo	ole No: pth: led: y:	TB-5 S-4 10.0 5/2/2016 001174 Galalina Pump Station & Storm Sewer		
Other Test	Results			
Description		Method	Result	Limits
Dispersion of Dispersion the Dispersion the Dispersion to Dispersion the Dispersion the Dispersion to Dispersion t	device	f Soils - Sieve & Hydrometer [ASTM D 422 - 07]	SOIL MIXER 1 MINUTE	
Hardness Date Te	stad		5/16/2016	
	ontent and D ontent (%) / (lb/ft ³)	Dry Density [ASTM D 2216 - 05]	19.1	
Date Te			5/12/2016	
Comments				
N/A				



Aggre	gate/Soil	Test Repo	ort			Report No: N	MAT:86-160105-	200-S009 Issue No: 1
Client:	City of Eastlake					Associatio Officials (ratory is accredited by the A on of State Highway and Tr AASHTO). The tests repor	ansportation ted have been
Project:	Galalina PS and Geotechnical Inv	Sewer Improvements restigation			A	AASHTO R18	d in accordance with the ter 3 cera k Payo	Λ
Job No:	86-160105-200						Issue: 5/19/2016 ed Signatory: Zeerak Pa	ydawy
Sample De	etails							
Boring No: Field Samp Sample De Date Samp Sampled B LWO No: Sample Lo	ble No: pth: led: y:	TB-6 S-4 10.0 5/2/2016 001174 Galalina Pump Sta	tion & Sto	rm Sewer		Sample Desc	cription:	
Particle S	ize Distribution					Grading: Particle Size Drying by:	e Analysis of Soils - Sieve & Hydrometer [ASTM D 42	12 - 07]
% Pas 100 - · · 90 - · · 80 - · · 70 - · · 60 - · · 50 - · · 40 - · · 20 - · · 10 - · ·		Sieve	45.1 µm 32.6 µm 21.1 µm 15.1 µm	8.5.1 µm 6.4 µm 3.2 µm 3.2 µm	1.3 µm + 1 : : : : : : : : : : : : : : : :	Date Tested: Sieve Size 1in 3/8in No.4 No.10 No.20 No.40 No.20 No.40 No.60 No.100 No.200 45.1 µm 32.6 µm 21.1 µm 15.1 µm 12.5 µm 6.4 µm 3.2 µm 1.3 µm	5/16/2016 % Passing 100 100 95 82 72 66 51 28 21 19.3 17.3 14.9 12.9 11.7 9.6 8.0 6.4 6.0 3.6	Limits
COBBLES	GRAVEL	SAND		FINE	S			
(0.0%)	Coarse Fine (0.0%) (5.0%)	Coarse (13.0%) Medium (16.0%)	Fine (45.0%)	Silt (14.2%)	Clay (6.8%)			



Aggree	gate/S	oil Test Report	Report No: MAT:8	6-160105-200-S009 Issue No: 1
Client:	City of East	ilake	Association of State	ccredited by the American Highway and Transportation
Project:	Galalina PS and Sewer Improvements Geotechnical Investigation		Officials (AASHTO). The tests reported ha completed in accordance with the terms of 3 cere & Day chary	
Job No:	86-160105	-200	Date of Issue: Approved Signat	5/19/2016 ory: Zeerak Paydawy
Sample Deta	ails			
Boring No: Field Sample Sample Dep Date Sample Sampled By LWO No: Sample Loca	th: ed: :	TB-6 S-4 10.0 5/2/2016 001174 Galalina Pump Station & Storm Sewer		
Other Test F	Results			
Description		Method	Result	Limits
Particle Size Analysis of Soils - Sieve & Hydrometer [ASTM D 422 - 07] Dispersion device Dispersion time (min) Shape Hardness		SOIL MIXER 1 MINUTE		
Moisture Con Wet Density (Dry Density (I	tent and Dry tent (%) (lb/ft ³) lb/ft ³)	Density [ASTM D 2216 - 05]	5/16/2016 23.9	
Date Test	ted		5/12/2016	
Comments				
N/A				



Agaro	lio2/ater	Test Report		Report No: MAT:86-160105-200-S006
	-	rest Kepult		Issue No: 1 This laboratory is accredited by the American
Client:	City of Eastlake			Association of State Highway and Transportation Officials (AASHTO). The tests reported have been
Project:	Galalina PS and Geotechnical Inv	Sewer Improvements estigation	4	ARSHTO RIS
Job No:	86-160105-200			Date of Issue: 5/19/2016 Approved Signatory: Zeerak Paydawy
Sample Det	ails			
Boring No: Field Sample Sample Dep Date Sampl Sampled By LWO No: Sample Loc	oth: ed: /:	TB-9 S-3 7.5 5/2/2016 001174 Galalina Pump Station & Stor	m Sewer	Sample Description:
Particle Si	ze Distribution			Grading: Particle Size Analysis of Sole - Sieve & Hydrometer (ASTM D 422 - 07)
				Drying by: Date Tested: 5/16/2016
% Passi	ing			
$100 - \cdots$ $90 - \cdots$ $80 - \cdots$ $60 - \cdots$ $50 - \cdots$ $40 - \cdots$ $30 - \cdots$ $10 - \cdots$ 0	3/8in 3/8in No.4	No.10 No.10 No.100 No.100 No.100 No.200 No.100 No.200 No.100 No.200 No.100 No.100 No.2	8.3 µm 6.1 µm 3 µm 1.3 µm	Sieve Size% PassingLimits1in100 $%$ in100 $3/8$ in100No.4100No.10100No.20100No.4099No.6099No.10098No.2009736.1 μ m90.326.7 μ m81.617.9 μ m68.013.5 μ m55.411.3 μ m47.68.3 μ m36.96.1 μ m27.24.4 μ m21.43.0 μ m16.51.3 μ m9.7
COBBLES	GRAVEL	SAND	FINES	
	Coarse Fine (0.0%) (0.0%)	Coarse (0.0%) Medium (1.0%) Fine (2.0%)	Silt Clay (73.6%) (23.4%)	



Telephone: 248.553.6300 Fax: 734.524.0927

		Poport No: MAT:	26 160105 200 S006
Aggrega	te/Soil Test Report	Report No. MAT.	6-160105-200-S006 Issue No: 1
	ty of Eastlake	Association of Stat	ccredited by the American e Highway and Transportation). The tests reported have been
=	alalina PS and Sewer Improvements eotechnical Investigation	completed in accor	dance with the terms of the neval pay chury
Job No: 86	5-160105-200	Date of Issue: Approved Signa	5/19/2016 tory: Zeerak Paydawy
Sample Details			
Boring No: Field Sample No Sample Depth: Date Sampled: Sampled By: LWO No: Sample Location	7.5 5/2/2016 001174		
Other Test Res	ults		
Description	Method	Result	Limits
Dispersion device Dispersion time (Shape		SOIL MIXER 1 MINUTE	
Hardness Date Tested		5/16/2016	
Ash Content (%) Organic Content Furnace Tempera Moisture Content	ature (°C)	93.8 6.2 440 66.0 oven-dried mass	
Moisture Content		Α	
Ash Content Met	hod (C or D)	С	
Date Tested		5/16/2016	
Moisture Content Wet Density (lb/ft	3)	66.0	
Date Tested	,	5/12/2016	
Moisture Content Wet Density (lb/ft Dry Density (lb/ft Date Tested	(%) ³)		
Comments			

* Unaccredited test method



			Depart No. MAT-00 400405 000 0007
Aaare	aate/Soil	Test Report	Report No: MAT:86-160105-200-S007
Client:	City of Eastlake		This laboratory is accredited by the American
Chent.	City of Eastlake		Association of State Highway and Transportation Officials (AASHTO). The tests reported have been completed in accordance with the terms of the
Project:		Sewer Improvements	3 cera k pay cary
	Geotechnical Inv	restigation	AASHTO R18
Job No:	86-160105-200		Date of Issue: 5/19/2016 Approved Signatory: Zeerak Paydawy
Sample De	etails		
Boring No:		ТВ-9	
Field Samp		S-4	
Sample De Date Samp		10.0 5/2/2016	
Sampled B			
LWO No: Sample Lo	cation:	001174 Galalina Pump Station & Storm Sewer	
	cation.	Calaina r unp Station & Storm Sewer	Sample Description:
			Grading: Particle Size Analysis of Solis - Sieve & Wash#200 (ASTM D 422 - 07)
Particle Si	ize Distribution		Drying by:
			Date Tested: 5/16/2016
0/ D	- 1		
% Pass 100 ⊤ · ·	sing 		
-	\mathbf{N}		Sieve Size % Passing Limits
90+••	\mathbf{X}		3/in 92
80 + • •	····· \	•••••••••••••••••••••••••••••••••••••••	3/8in 77 No.4 53
70 - • •	· · · · · · · · · · · · · · · · · · ·		···· No.10 34
60 + · ·	\sim		No.20 24
			No.40 15 No.60 11
50+	• • • • • • • • • • • • • • • • • • • •	X	No.100 9
40 - • •			No.200 8 Finar No.200 (75µm) 8
30+••			Finer No.200 (75µm) 8
-			
20+			
10 - • •		······	
0		4 0 0 0 0 0 0	
	1 in 34 in 378 in	No.40 No.20 No.40 No.200 No.200	
		Sieve	
COBBLES	GRAVEL	SAND FINES (8	3.0%)
(0.0%)	Coarse Fine (8.0%) (39.0%)	Coarse (19.0%)Medium (19.0%)Fine (7.0%)Silt	Clay
			11



\mathbf{r}					
Aggrega	ate/Soil Test Report	Report No: MAT:86-160105-200-S007 Issue No: 1			
Client: C	City of Eastlake	This laboratory is accredited by the American Association of State Highway and Transportation			
	Salalina PS and Sewer Improvements Geotechnical Investigation	Officials (AASHTO). The tests reported have been completed in accordance with the terms of the ABHTO RIS			
Job No: 8	36-160105-200	Date of Issue: 5/19/2016 Approved Signatory: Zeerak Paydawy			
Sample Details	5				
Boring No: Field Sample N Sample Depth: Date Sampled: Sampled By: LWO No: Sample Locatio	10.0 5/2/2016 001174				
Other Test Re	sults				
Description	Method	Result Limits			
Dispersion devic Dispersion time Shape Hardness Date Tested	(min)	5/16/2016			
Moisture Conter Wet Density (lb/	nt (%) [ft ³]	14.5			
Dry Density (lb/f Date Tested		5/12/2016			
Comments					
Comments					
N/A					



Aggre	gate/Soil	Test Report	Report No: MAT:86-160105-200-S002 Issue No: 1
Client: Project:	City of Eastlake Galalina PS and	Sewer Improvements	This laboratory is accredited by the American Association of State Highway and Transportation Officials (AASHTO). The tests reported have been completed in accordance with the terms of the
	Geotechnical Inv	estigation	ARASHTO RIB 3 CECAN Day chary
Job No:	86-160105-200		Date of Issue: 5/19/2016 Approved Signatory: Zeerak Paydawy
Sample De	etails		
Boring No: Field Samp Sample De Date Samp Sampled B LWO No: Sample Lo	ble No: pth: led: y:	TB-11 S-4 10.0 5/2/2016 001174 Galalina Pump Station & Storm Sewe	ver Sample Description:
			Grading: Particle Size Analysis of Sola - Sleve & Hydrometer (ASTM D 422 - 07)
Particle Si	ize Distribution		Drying by: Date Tested: 5/16/2016
$ \begin{array}{c} 100 & - \\ 90 & - \\ 80 & - \\ 70 & - \\ 60 & - \\ 50 & - \\ 40 & - \\ 30 & - \\ 20 & - \\ 10 & - \\ 0 & - \\ \end{array} $	3/8in 3/8in No.4	Sieve	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
COBBLES	GRAVEL	SAND F	FINES
(0.0%)	Coarse Fine (0.0%) (0.0%)	Coarse (0.0%) Medium (3.0%) Fine (26.0%) Silt (55.1%)	Clay (15.9%)



Aggree	gate/Soil Test Report	Report No: MAT:8	6-160105-200-S0 Issue No
Client:	City of Eastlake		ccredited by the American Highway and Transportation
Project:	Galalina PS and Sewer Improvements Geotechnical Investigation	completed in accord	The tests reported have be lance with the terms of the e_{M} $P^{a\gamma}$ d_{M}
Job No:	86-160105-200	Date of Issue: 5 Approved Signat	5/19/2016 ory: Zeerak Paydawy
ample Det	ails		
Boring No: Field Sampl Sample Dep Date Sample Sampled By LWO No: Sample Loc	oth: 10.0 ed: 5/2/2016 ': 001174		
Other Test	Results	Result	Limits
Particle Size Dispersion de Dispersion til Shape	Analysis of Soils - Sieve & Hydrometer [ASTM D 422 - 07] evice	SOIL MIXER 1 MINUTE	2
Hardness Date Tes		5/16/2016	
Moisture Cor Moisture Cor Wet Density Dry Density ((lb/ft ³)	41.5	
Date Tes	ted h and Organic Content [ASTM D 2974 - 07]*	5/12/2016	
Ash Content Organic Con	(%) tent (%)	95.6 4.4	
Moisture Cor Moisture con	tents are proportioned by	440 42.0 oven-dried mass	
	ntent Method (A or B) Method (C or D)	A C 5/16/2016	



		Report No: MAT:86-160105-200-S003
Aggreg	ate/Soil Test Report	Issue No: 1
Client:	City of Eastlake	This laboratory is accredited by the American Association of State Highway and Transportation Officials (AASHTO). The tests reported have been
Project:	Galalina PS and Sewer Improvements Geotechnical Investigation	completed in accordance with the terms of the 3 cere R Pay Carry
Job No:	86-160105-200	Date of Issue: 5/19/2016 Approved Signatory: Zeerak Paydawy
Sample Deta	ils	
Boring No: Field Sample Sample Depti Date Sampled Sampled By: LWO No:	h: 20.0 d: 5/2/2016 001174	
Sample Loca	tion: Galalina Pump Station & Storm Sewer	Sample Description:
		Grading
Particle Size	e Distribution	Grading: Particle Size Analysis of Solis - Sieve & Wash#200 [ASTM D 422 - 07] Drying by:
		Date Tested: 5/16/2016
% Passing		
100 - · · · · · 90 - · · · · · 80 - · · · · 60 - · · · · 50 - · · · · 40 - · · · · 30 - · · · · 10 - · · · ·	Sieve	Sieve Size % Passing Limits 1in 100 ¾in 95 3/8in 83 No.4 65 No.10 43 No.20 28 No.40 20 No.60 16 No.100 13 No.200 11 Finer No.200 (75µm) 10
COBBLES	GRAVEL SAND FINES (11.0%)	$\exists \parallel$
	parse 5.0%)Fine (30.0%)Coarse (22.0%)Medium (23.0%)Fine (9.0%)SiltClay	



\checkmark						
Aggregate/	Soil Test Report	Report No: MAT:86	S-160105-200-S003 Issue No: 1			
Client: City of E	astlake	Association of State I	redited by the American Highway and Transportation			
	PS and Sewer Improvements nical Investigation	Officials (AASHTO). The tests reported have been completed in accordance with the terms of the 3 cent Part dawy				
Job No: 86-1601	05-200	Date of Issue: 5/19/2016 Approved Signatory: Zeerak Paydawy				
Sample Details						
Boring No: Field Sample No: Sample Depth: Date Sampled: Sampled By: LWO No: Sample Location:	TB-11 S-6 20.0 5/2/2016 001174 Galalina Pump Station & Storm Sewer					
Other Test Results						
Description	Method	Result	Limits			
Moisture Content and D	Dry Density [ASTM D 2216 - 05]					
Moisture Content (%) Wet Density (lb/ft ³) Dry Density (lb/ft ³)		12.8				
Date Tested		5/12/2016				
Particle Size Analysis of Dispersion device Dispersion time (min) Shape Hardness	f Soils - Sieve & Wash#200 [ASTM D 422 - 07]					
Date Tested		5/16/2016				
Comments						
Comments						
N/A						

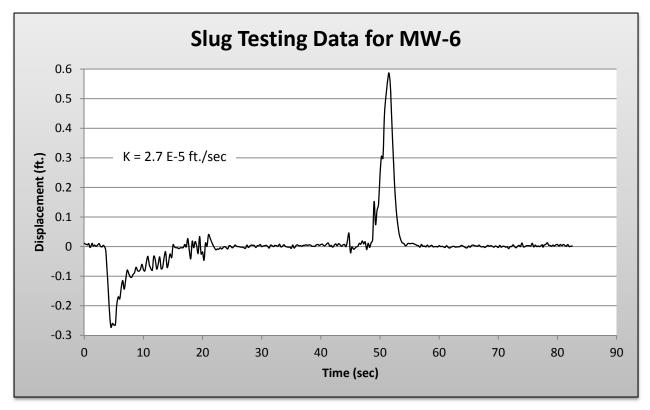


Figure No. 21

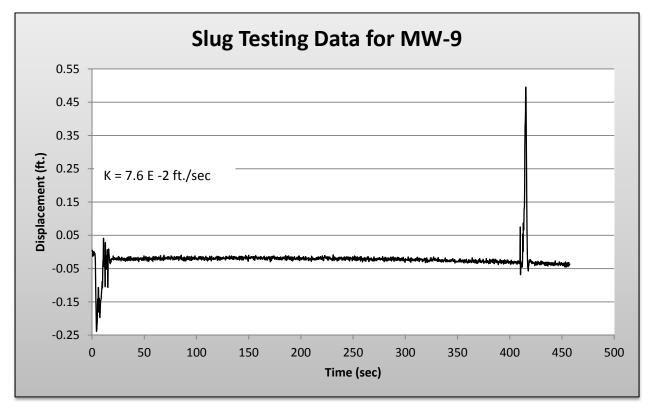


Figure No. 22

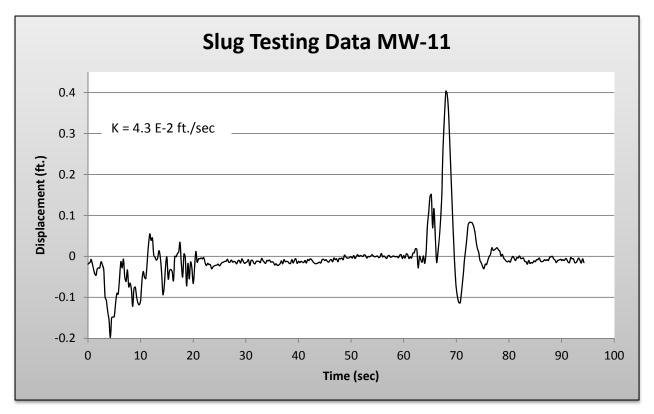


Figure No. 23

MONITORING WELL: MW-6

Project Name: Galalina PS Sewer

Project Location: Eastlake, OH



NTH Consultants, Ltd. NTH Proj. No.: 86-160105

Checked By:

LOG OF MONITORING WELL							WATER LEVEL DAT					
			SUBSURFACE PROFILE				LATION	SCHEMATIC	DATE	ELEV (FT)	Depth	
							то	P OF WELL	5/18/201	16 572.4	3.4 feet	
ELEV. (FT)	PRO- FILE	ELEV	GROUND SURFACE ELEVATION: 576.0	DEPTH	DEPTH (FT)	Well Detail	CASIN	IG ELEVATION: 575.8 ft	5/27/20	16 572.6	3.2 feet	
							010.0 h		5/18/201	16 571.4	4.4 feet	
_	112.61	E75.0		0.0	4	2 5 2 5			0.0			
575	X	575.6	ASPHALT	0.4	-							
-	X		Very Stiff Gray SILTY CLAY				Cor	ment Grout				
-		573.0		3.0	-							
			Medium Gray SILTY CLAY		- 5				5.0			
570	XI	1	Medium Gray SILTT CLAT									
_	Ч	569.5		6.5	E		Bent	tonite Slurry				
_	1				L				8.0			
_					L			Sand				
-	1		Vanil and Crou SILTY SAND		10				10.0			
565	1.		Very Loose Gray SILTY SAND, Trace Clay and Gravel		-							
-	,1				-			Sand		-		
-	1				-							
	1	561.0		15.0	15				15.0			
560			END OF BORING AT 15.0 FEET.									
_												
_												
-												
555_												
-												
550												
_												
_												
-												
- 545												
										_		
	-											
Inspe Cont Drille	llatio ector racto er:	on Date :: or:	e: 15.0 FT 5/5/2016 A. Fazio Ohio TestBor, Inc. D. Hepner			Casing Dian Casing Leng Casing Type Tip Elevatio GPS Coordi	gth: e: n:	2" 5' PVC				
Equipment: Notes:		nt:	2 1/4" HSA Mobile track-mounted rig			Screen Diameter: Screen Length: Screen Mesh: Screen Type:		2" 10' SLOTTED PVC	п			
						Well Type: Mo		MONITOR	MONITORING WELL		Figure No. 24	

MONITORING WELL: MW-9

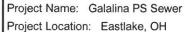


NTH Consultants, Ltd. NTH Proj. No.: 86-160105 Checked By: NTH Proj. No.: 86-160105

Project Name: Galalina PS Sewer Project Location: Eastlake OH

-									<u>O</u>	Checked B		
				LOG OF MONITORI	NGV	VEL		171011			DEPTH	
		T	-	SUBSURFACE PROFILE			INSTAL	LATION S	SCHEMATIC	DATE	ELEV (FT)	Depth
ELEV.	PRO-			GROUND		DEPTH	Well	то	P OF WELL	5/18/2016	573.7	2.1 feet
(FT)	FILE	ELEV	/	SURFACE ELEVATION: 576.0	DEPTH	(FT)	Detail	CASIN	G ELEVATION: 575.8 ft	5/27/2016	573.95	1.85 feet
_				the state and state and state and the						5/18/2016	573.6	2.2 feet
-					0.0		CAN LOAR		0	0		
575		575.0)	ASPHALT	1.0	_	000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0					
	M			Medium Gray SILTY CLAY		_	P b b P b P b P b P b P b P b P b P b P					
-	H,	573.0)		3.0	-		Cer	ment Grout			
) (J .	K											
-	VI			Very Soft Gray CLAYEY SILT,		5			5	0		
570	1X			Trace Sand, Trace Organics		-	- 68	Bent	tonite Slurry			
-	44	568.5	5		7.5	-		Dem				
80		2				-			8	0		
13		-		Loose Dark Gray SANDY		10	- 161 169	Fi	Iter Sand	0		
- 565				GRAVEL, Trace Clay		- 10	1 📄		10	<u> </u>		
000		564.0)		12.0	_	1 🗐					
-	1					_	1 目	Fi	Iter Sand			
_	1			Loose Dark Gray SILTY SAND		_	1 =					
	1	561.0			15.0	15	1 =		15	0		
560				END OF BORING AT 15.0 FEET							Contra de Califica	
12												
-												
-												
-												
555												
-												
-												
-												
-												
550												
-												
-												
-												
- 545												
1. 												
Tota	I Dep	oth:		15.0 FT			Casing Dian	neter:	2"			
	ector	on Da ':	ate:	5/5/2016 A. Fazio			Casing Leng Casing Type	gth: e:	5' PVC			
Con	tracto			Ohio TestBor, Inc.			Tip Elevatio	n:	6 BUITU			
Drill Equi	er: pme	nt:		D. Hepner	mounte		GPS Coordi	nates:				
				2 1/4" HSA Mobile track-	nounte	1040	Screen Dian		2"			
Note	s:						Screen Leng Screen Mes	gth: h:	10' SLOTTED"			
							Screen Type		PVC			
							Well Type:		MONITORING WELL			
											Fi	gure No. 2

MONITORING WELL: MW-11



NTH Consultants, Ltd.

NTH Proj. No.; 86-160105

Checked By:

LOG OF MONITORING WELL WATER LEVEL DATA SUBSURFACE PROFILE INSTALLATION SCHEMATIC DATE ELEV (FT) Depth 5/18/2016 573.8 2 feet TOP OF WELL CASING ELEVATION: 575.8 ft GROUND Well ELEV. PRO-FILE DEPTH ELEV DEPTH 5/27/2016 574.2 1.6 feet (FT) (FT) SURFACE ELEVATION: 576.0 Detail 5/18/2016 573.6 2.2 feet 0.0 0.0 575.5 0.5 **Topsoil CLAYEY SILT** 575 FILL: Medium Compact Brown CLAYEY SILT, Trace Sand 573.0 3.0 Medium Gray SILTY CLAY, Trace Sand 5 570.5 5.5 Cement Grout 570 Very Soft Gray SANDY SILT, Little Clay 10 565 11.0 564.0 12.0 Bentonite Slurry 14.0 Loose Gray SAND, Trace Sand 15 15.0 GRAVEL 560 559.0 17.0 0 5.0 20 Medium Compact Gray Sand 555 **GRAVELLY SAND, Trace Clay** and Silt 00 551.5 24.5 25 25.0 Gray SILTY CLAY 550 END OF BORING AT 25.0 FEET. MONITORING WELL LOG MW 86-160105.GPJ NTH CORPORATE.GDT 6/16/16 545 Total Depth: **Casing Diameter:** 2" 25.0 FT Casing Length: Installation Date: 15' 5/5/2016 Inspector: PVC Casing Type: A. Fazio Contractor: Tip Elevation: Ohio TestBor, Inc. Driller: **GPS Coordinates:** D. Hepner Equipment: 2 1/4" HSA Mobile track-mounted rig Screen Diameter: 2" 10' Screen Length: Notes: Screen Mesh: SLOTTED" Screen Type: PVC Well Type: MONITORING WELL Figure No. 26